EMMA4Drive – A dynamic human model for autonomous driving (2021 – 2024)

Joachim Linn, Monika Harant, Michael Roller, Marius Obentheuer, René Reinhard, Michael Kleer (Fraunhofer Institut für Techno- und Wirtschaftsmathematik ITWM, Kaiserslautern)

Jörg Fehr, Niklas Fahse, Fabian Kempter (Institut für Technische und Numerische Mechanik ITM, Universität Stuttgart)

Michael Koch, Daniel Dengel (fleXstructures GmbH, Kaiserslautern)

35. Forum "Simulation in der Automobilindustrie", Fraunhofer ITWM, 3. Mai 2024

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EMMA4Drive – A typical application case and project goals

Automated Driving

- Driver is passively sitting in the car (most of the time)
- Driver suddenly has to take control of the car in certain "dynamic" driving situations

Project Goals

- Simulate realistic human motions of the "virtual driver", e.g. in such "passive to active" transitions, during dynamic driving situations
- Driver-seat interaction: Modeling and efficient computation
- Consider increasing variability of driving situations, postures and body sizes for ergonomic and safety-critical protection in automated vehicle concepts











The EMMA4Drive project consortium



Jniversity of Stuttgart Institute of Engineering and Computational Mechanics (ITM)



Model order reduction (MOR) of contact interaction between human and seat

Expertise:

- FEM simulation of humans in crash and pre-crash situations
- Model order reduction (MOR) methods





Include driver seat interaction in motion generation using optimal control methods

Expertise:

- Biomechanical multibody dynamics modeling of humans
- Motion generation by optimal control of muscle actuated multibody DHM





Link to the automotive industry Definition of software requirements

Expertise:

- maintenance and distribution of the IPS software, including IPS IMMA (a DHM for digital factory applications)
- New module: IPS Virtual Driver





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EMMA4Drive: Positioning within the automotive DHM landscape

- Active behavior of passenger is relevant in many driving scenarios and is crucial for the initial position of crash phase
- With the rise of automated driving capabilities, the vehicle and its occupants need to be considered as a whole
- Comfort and safety in automated vehicles needs to be evaluated for new seating positions

N. Fahse et al.: *Dynamic Human Body Models in Vehicle Safety - An Overview*, GAMM Mitteilungen, Vol. **46** (2), Juni 2023





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The Digital Human Model EMMA

A biomechanical multibody system

- EMMA is a biomechanical multibody dynamics model with a kinematic tree structure and a system of joints and actuation elements modeling the musculoskeletal system of the humar body
- Different actuation mechanisms are possible:
 - Torque Generators (Motors)
 - Muscle Torque Generators (MTG)
 - Hill-type muscles
- EMMA provides motion generation / prediction using an optimal control approach
- EMMA can handle rigid contacts
- Aim of EMMA4Drive: Soft Contact Modeling



Optimal Control for Motion Generation



 $\min J(\boldsymbol{q}(t), \boldsymbol{u}(t))$

 $0 = \ddot{\boldsymbol{q}}(t) - \boldsymbol{f}(\boldsymbol{q}(t), \dot{\boldsymbol{q}}(t), \boldsymbol{u}(t), \boldsymbol{\lambda}(t))$ $0 = \boldsymbol{g}(\boldsymbol{q}(t))$

 $0 = e(\boldsymbol{q}(t), \boldsymbol{u}(t))$

 $0 \le c(\boldsymbol{q}(t))$

 $\begin{aligned} \boldsymbol{q}_{-} &\leq \boldsymbol{q}(t) \leq \boldsymbol{q}_{+} \\ \boldsymbol{u}_{-} &\leq \boldsymbol{u}(t) \leq \boldsymbol{u}_{+} \end{aligned}$

Rigid Multibody System



Muscle (Torque Generator) Modelling







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Rigid (& Soft) Contact Modeling

EMMA

The Digital Human Model EMMA

Muscle Torque Generators – New form of actuation

Muscle Torque Generators (MTG):

- One MTG represents the muscular properties for the deflection of a limb in one direction.
- Position- and velocity-torque relationship similar to muscle models, but at joint angle level, with rigid tendon.

•
$$\tau^{MTG} = af^{A}(\Theta)f^{V}(\omega) + f^{PE}(\Theta)\left(1 - \beta^{PE}\frac{\omega}{\omega_{max}}\right)$$

a: MTG activation, β^{PE} : damping term

- MTGs are available in EMMA for multiple joints.
- The available set of MTGs is currently extended by performing and evaluating experimental data (2 ongoing master theses at the RPTU Kaiserslautern).









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EMMA: Motion generation by discrete Lagrangian mechanics and optimal control with constraints

The motion for the EMMA model is obtained by solving a (multiphase) optimal control problem:

- Minimizing a cost function and fulfilling the equation of motion and constraints
- Includes actuation models
- Includes contacts with the environment
- Constraints describe the outline of the motion:
- O Start/End position and velocity
- Start and contact loss
- O Collision avoidance

 $\min_{q,\dot{q},\lambda,u} J(q,\dot{q},\lambda,u) := \sum_{i=0}^{N} \int_{t_i}^{t_{i+1}} \phi(q,\dot{q},\lambda,u) dt$ $\frac{\partial}{\partial q}L(q,\dot{q}) - \frac{\partial}{\partial t}\frac{\partial}{\partial \dot{q}}L(q,\dot{q}) - G_{\dot{t}}(q)^{T}\lambda + f(q,\dot{q},u) = 0$ q(q) = 0 $h_i(q, \dot{q}, \lambda, u) \ge 0$ $e_i(q, \dot{q}, \lambda, u) = 0, \qquad i = 0, \dots, N$ $q_{-} \leq q \leq q_{+}, \ \dot{q} \leq \dot{q} \leq \dot{q}_{+},$ $u_{-} \leq u \leq u_{+}$, $\lambda_{-} \leq \lambda \leq \lambda_{+}$







EMMA

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Optimal Control

DMOCC (discrete mechanics and optimal control for constrained systems)



- Variational integrator to solve the constrained equation of motions in time
- Discretization is already applied to the Lagranged'Alembert principle, and the variation is applied to the discrete equations
- Structure preserving
- Advantages: big step sizes are possible, no numerical drift
- The resulting NLP is solved with the Interior Point Method provided by IPOPT

$$\min \sum_{l=0}^{N-1} \phi_d(q^l, q^{l+1}, u^l, u^{l+1})$$

 $\min J(\boldsymbol{q}(t), \boldsymbol{u}(t))$

 $\begin{aligned} 0 &= \ddot{q}(t) - f(q(t), \dot{q}(t), u(t), \lambda(t)) \\ 0 &= g(q(t)) \\ 0 &= e(q(t), u(t)) \\ 0 &\leq c(q(t)) \\ q_{-} &\leq q(t) \leq q_{+} \\ u_{-} &\leq u(t) \leq u_{+} \end{aligned}$

Lagrange –d'Alembert principle:

$$\begin{split} \delta \int L(q,\dot{q}) + g(q) \cdot \lambda dt &+ \int F(q,\dot{q},u) \cdot \delta q dt = 0 \\ \text{Discretizing } \begin{bmatrix} t_o, t_f \end{bmatrix} \text{ in intervals} \\ \text{with fixed step size } h &= \frac{t_f - t_o}{N} \end{split} \\ \int_{t_l}^{t_{l+1}} L(q,\dot{q}) dt \approx L_d(q^l,q^{l+1}) \\ \int_{t_l}^{t_{l+1}} g(q) \cdot \lambda dt \approx \frac{h}{2} (g(q^l) \cdot \lambda^l + g(q^{l+1}) \cdot \lambda^{l+1}) \\ \int_{t_l}^{t_{l+1}} F(q,\dot{q},u) \cdot \delta q dt \approx F_d^-(q^l,q^{l+1},u^l,u^{l+1}) \cdot \delta q^l \\ &+ F_d^+(q^l,q^{l+1},u^l,u^{l+1}) \cdot \delta q^{l+1} \end{split}$$

$$\partial_{2}L_{d}(q^{l-1},q^{l}) + \partial_{1}L_{d}(q^{l},q^{l+1}) + F_{d}^{-}(q^{l},q^{l+1},u^{l},u^{l+1}) + F_{d}^{+}(q^{l},q^{l+1},u^{l},u^{l+1}) - hG^{T}(q^{l})\lambda^{l} = 0, \qquad l = 0, \dots, N-1 \\ g(q^{l}) = 0, \qquad l = 0, \dots, N \qquad [S. Leyendecker et al. Optim. control \\ C_{-} \leq c(q^{l},u^{J},\lambda^{K}) \leq c_{+} \qquad Appl. Methods, 31(6), 505-528, 201$$

Appl. Methods, 31(6), 505–528, 2010]





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Discretizing objective ϕ

and constraints *c*

Motion generation without MoCap by Discrete Mechanics & Optimal Control







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Simulation of a breaking manoeuvre with the EMMA model

Model:

- Each arm:
 - 29 Hill-type muscles
 - 7 degrees of freedom
- Hip, knees, knuckles, lower back, neck controlled by joint torques
- Buttocks fixed to seat
- Hands fixed to steering wheel
- Feet fixed to pedals

Optimal Control Setup:

- Constantly accelerated to 5m/s
- Sudden break to 0 m/s
- Rest to rest
- Minimize Control











THUMS Model Transfer

THUMS-based RMBS Model

- Export of the skeleton segments
- Setup of the model using the coordinate systems proposed by the EU-project "Piper"
- Definition of the joints based on the old model
- Implementation of new joints in EMMA
- Read-in of the LSDyna-output of the THUMS occupant model in the "neutral" state: mass, CoM, inertia tensors
- Manual assignment of each FE object to the segments of the RMBS model EMMA
- Automatic Transfer of the dynamic parameters to the EMMA model including merging of all FE objects that belong to one segment



The occupant version as EMMA model. The position of the red spheres represents the position of the FE objects' center of masses.



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EMMA4Drive: Simulation of a steering wheel takeover

Simulation of a steering wheel takeover

- Initial Position: "Zero Gravity"
- Final Position: Hands on the steering wheel
- Two simulation scenarios: with and without a powered seat
- Back and seat are coupled by 2 linear springs
- The driver is rigidly connected at the lower limb
- The motion is predicted by minimizing a combination of
 - Control & control change effort
 - Duration
 - Kinetic Energy Ο

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Simulation of safe optimal braking in a shuttle bus

THUMS-based RMBS Model (Industry project with ZF Friedrichshafen)

Simulation Scenario

- A passenger is standing in an autonomous-driven bus,
- may hold or not hold onto a vertical handrail,
- has to balance a sudden braking maneuver:
 - Piecewise linear acceleration profile
 - Acceleration profile is prescribed or optimized

Project Goal

- Comfort and safety studies: What is an optimal brake profile for the bus so that
 - The bus comes to a stop quickly
 - The Passenger's risk of injury is low



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EMMA4Drive: Simulation of safe optimal braking in a shuttle bus



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Simulation of safe optimal braking in a shuttle bus

F

Shuttle Passenger Simulation



Brake profile optimization of a passenger standing in driving direction without handrail support.



Brake profile optimization of a passenger standing in driving direction with handrail support.



A passenger standing opposite to the driving direction with handrail support balancing a prescribed braking maneuver.





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MOR: Efficient simulation of driver-seat interaction by surrogate models



- Capable of adequately representing the (complex) contact situation
- Runtime-efficient
- Able to represent closing and opening of contact
- Applicable in the optimal control setup: sufficiently smooth and automatically differentiable

Method:

 FE simulations provide realistic contact forces that are used to train NNs which can be included in EMMA

Focus on head and headrest to develop a robust and general method to obtain such contact models

Generation of Interaction Force Dataset

- High fidelity & long running
 FEM simulations
- Parameter variations

Optimal Control with Driver-Seat Interaction

- MBS simulations
- Evaluate ergonomics
- Simulate long scenarios
- Simulate active controlled movements









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Niklas Fahse University of Stuttgart

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EMMA Simulation vs. FE Simulation

- Current contact model is applied in EMMA
- EMMA simulation is performed
- The model's kinematics of the EMMA simulation is transferred to FE
- The contact forces of the FE simulation is evaluated and included in the training data









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Niklas Fahse University of Stuttgart

EMMA Simulation vs. FE Simulation

- Train MLP Regressor to learn interaction forces/torques from relative kinematics
- Split data pool into 70% training and 30% test data
- Evaluate training on test data:



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Convergence Evaluation and next steps

Compare contact forces/torques between the current contact model and FE simulations:

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- Deviation of contact forces/torques is reduced
- Lower reduction in the forces than in the moment because of non-ideal preliminary data

- 200 cycles
- Calculation time on a standard laptop: ~6 days

Niklas Fahse

University of Stuttgart

Force RMSE [N] — Moment RMSE [Nm]









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The RODOS driving simulator @ ITWM



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Experiments

for validation / additional data for Emma4Drive simulations

- Movement recordings during different driving maneuvers, positions and level of alertness of the driver
- Level of comfort, savety, and trust in the systems are rated by the subjects



Robot based driving simulator RODOS (@ ITWM)



Driver in the loop simulator/seat tilting device (ITM)





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Transfer of RODOS maneuvers to EMMA

Overview

Goal:

- Transfer the movement of the cabin during Rodos experiments to EMMA
- Predict driver movements with EMMA
- Compare EMMA movements with those of the subjects

Method:

- Actuator was implemented that allows for a direct control of the accerleration of a body
- Read-In and including an LSQ term for the IMU-Data







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Transfer of RODOS maneuvers to EMMA

First Simulation results

Simulation:

- EMMA Manikin based on THUMS skeleton was placed in the seat
- 2-Phase approach:
 - 1. Phase: no change in manikin actuation was allowed during the response time
 - 2. Phase: Manikin reacts to the maneuver of the car

Next steps:

- Compare movement with video data
- Adjust objective function
- Test simulation with NMPC approach







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EMMA4Drive – A dynamic human model supporting research and early phases in development for passenger safety concepts in autonomously driving vehicles

Goals of the EMMA4Drive project:

- Simulate realistic human motions of the "virtual driver", e.g. in such "passive to active" transitions, during dynamic driving situations
- Driver-seat interaction: Modeling and efficient computation
- Consider increasing variability of driving situations, postures and body sizes for ergonomic and safety-critical protection in automated vehicle concepts

Outcomes of the EMMA4Drive project:

- A box of software tools that support the development process of passenger safety concepts already in early phases ...
- ... and fill a gap in the current DHM landscape for applications in automotive engineering
- IPS Virtual Dynamic Driver: A new IPS software module for engineers in automotive industry













